



Use of a fully tensorial approach to characterize the stress variability at Forsmark

Bruno Figueiredo¹, J. Sjöberg¹ & D. Mas Ivars^{2,3}

¹ Itasca Consultants AB, Sweden

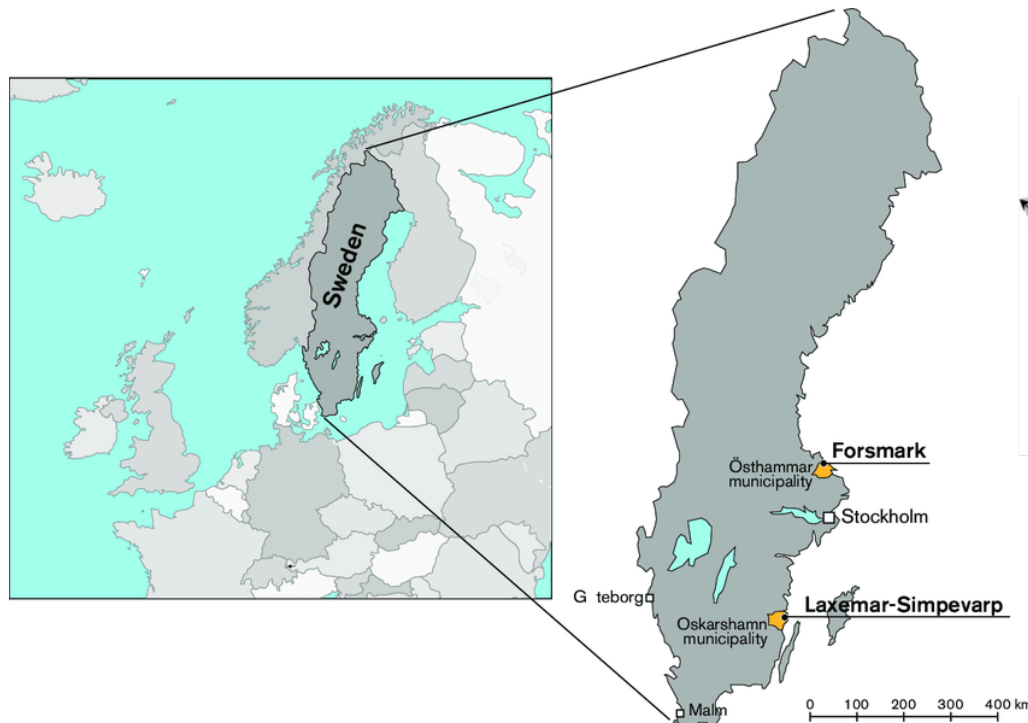
² SKB, Swedish Nuclear Fuel and Waste Management Company, Solna, Sweden

³ KTH, Royal Institute of Technology, Stockholm, Sweden

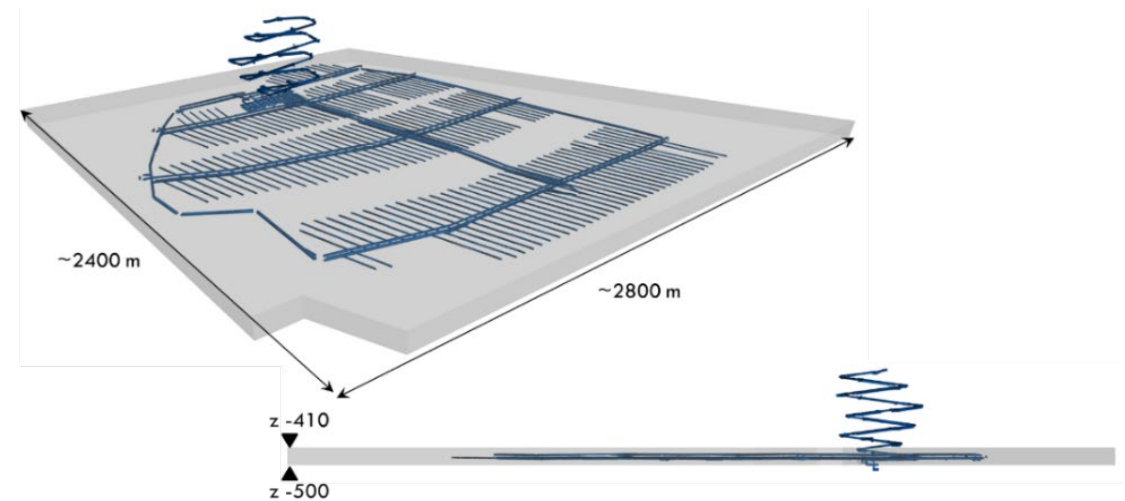
5th International Itasca Symposium, February 17-20, Vienna, Austria

Motivation (1/3)

- The Forsmark site is the chosen location for the repository for spent nuclear fuel in Sweden.
- The stress magnitude and orientation is an important factor in the design of the repository.



Location of Forsmark



Layout of the repository

Motivation (2/3)

- Scalar/vector approach - based on the separate evaluation of magnitudes and orientations
- Tensorial approach – based on the evaluation of the principal stress magnitude and orientation, obtained from the mean stress tensor

A scalar/vector approach is incorrect, because it leads to non-perpendicular principal stresses, violating the principle of continuum mechanics

| Depth [m] | Stress nr | Stress tensor components (MPa) | | | | | |
|-----------|----------------|--------------------------------|---------------|---------------|---------------|---------------|---------------|
| | | σ_{xx} | σ_{xy} | σ_{xz} | σ_{yy} | σ_{yz} | σ_{zz} |
| 416.55 | S ₁ | 43.2 | 4.7 | -3.4 | 32.7 | -0.3 | 15.3 |
| 416.57 | S ₂ | 41.2 | 6.6 | -3.3 | 31.3 | 0.5 | 17.7 |
| 416.60 | S3 | 42.9 | 8.8 | -4.0 | 35.8 | 2.8 | 14.6 |
| 416.62 | S4 | 45.1 | 5.4 | -4.4 | 31.6 | 2.3 | 18.3 |
| 416.68 | S5 | 42.6 | 4.4 | -1.9 | 28.3 | 0.8 | 15.1 |
| ... | ... | ... | ... | ... | ... | ... | ... |
| 417.17 | S17 | 29.7 | 3.0 | -4.9 | 40.5 | -0.1 | 14.2 |

Stress database

| Mean principal stress | σ_1 & σ_2 (°) | σ_2 & σ_3 (°) | σ_3 & σ_1 (°) |
|------------------------|-----------------------------|-----------------------------|-----------------------------|
| Scalar/vector approach | 10 | 86 | 85 |
| Tensorial approach | 90 | 90 | 90 |

Angle between principal stress directions

Motivation (3/3)

- Tensorial approaches can be divided in two sub-groups: quasi-tensorial and fully tensorial.
- ❖ Quasi-tensorial approaches are not adequate to assess the overall stress field dispersion, when the various stress tensor components are highly correlated.

| | σ_{xx} | σ_{xy} | σ_{xz} | σ_{yy} | σ_{yz} | σ_{zz} |
|---------------|---------------|---------------|---------------|---------------|---------------|---------------|
| σ_{xx} | 1.00 | 0.53 | 0.18 | -0.67 | 0.01 | 0.42 |
| σ_{xy} | 0.53 | 1.00 | 0.08 | -0.66 | -0.12 | 0.48 |
| σ_{xz} | 0.18 | 0.08 | 1.00 | -0.32 | -0.29 | -0.24 |
| σ_{yy} | -0.67 | -0.66 | -0.32 | 1.00 | 0.03 | -0.44 |
| σ_{yz} | 0.01 | -0.12 | -0.29 | 0.03 | 1.00 | 0.17 |
| σ_{zz} | 0.42 | 0.48 | -0.24 | -0.44 | 0.17 | 1.00 |

- ❖ Fully tensorial approaches take into account the stress correlation, but to an accurate estimation of the correlation coefficients, a minimum number of 7 data in a limited depth range of 50-100 m, must be available.

Tensorial approach

- Normal distribution of distinct stress components
 - ❖ Quasi-tensorial: Univariate normal distribution
 - ❖ Fully tensorial: Multivariate normal distribution (Gao & Harrison, 2018)

$$f_{sd} = \frac{1}{\sqrt{(2\pi)^{\frac{1}{2}p(p+1)}|\Omega|}} \exp\left(-\frac{1}{2}(s_d - m_d)^T(\Omega)^{-1}(s_d - m_d)\right),$$

Ω - covariance matrix

s_d - magnitude of the six distinct stress components

m_d - mean of the magnitude of the six distinct stress components

p – dimension of the stress tensor

- Effective variance: scalar value that measures the overall stress dispersion [MPa²]

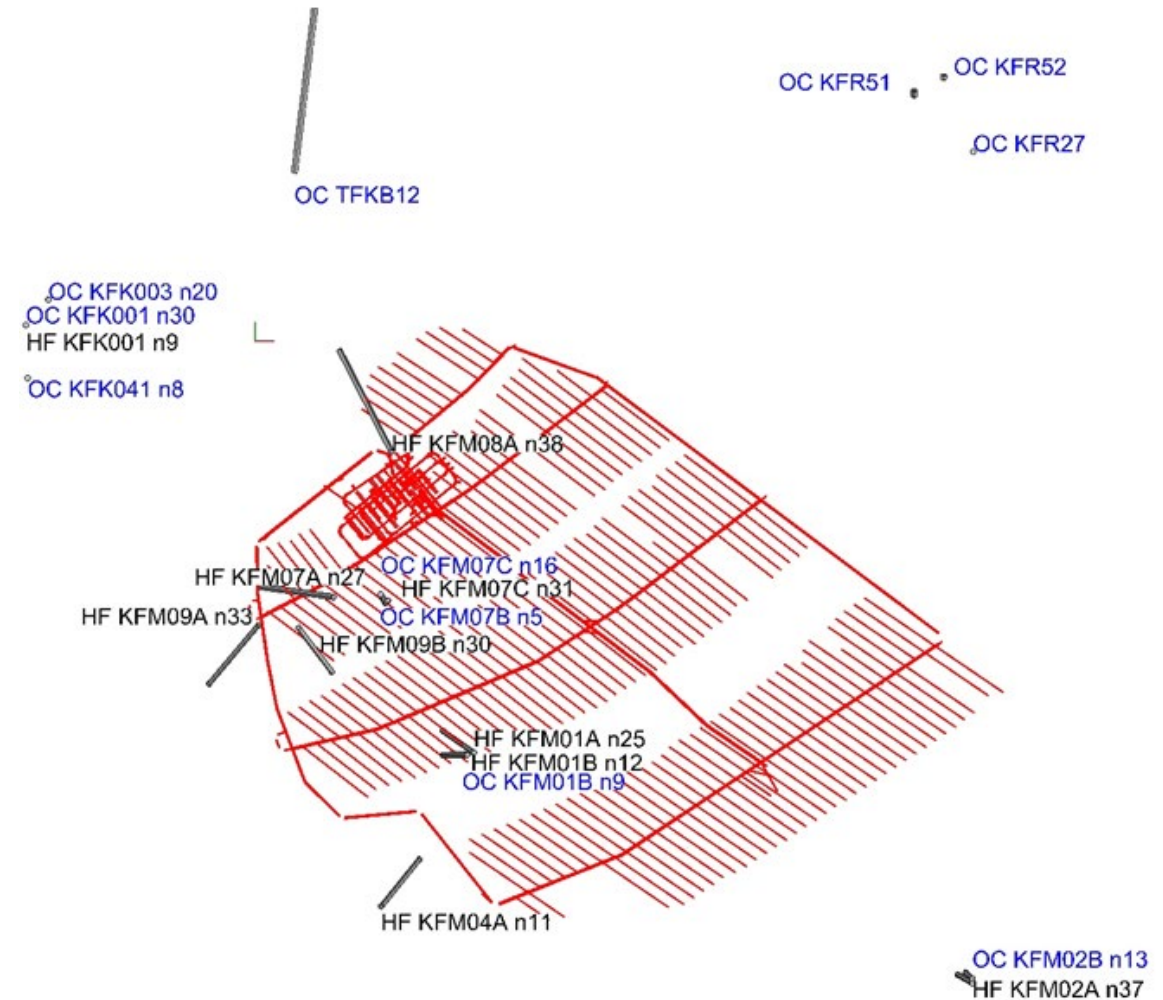
$$V_{eff} = \frac{1}{2}p(p+1)\sqrt{|\Omega|}$$

Gao, K. & Harrison, J. P. 2018. Multivariate distribution model for stress variability characterisation. *Int. J. Rock Mech. Min. Sci.*, 102: 144–154.

Application to stress measurement data

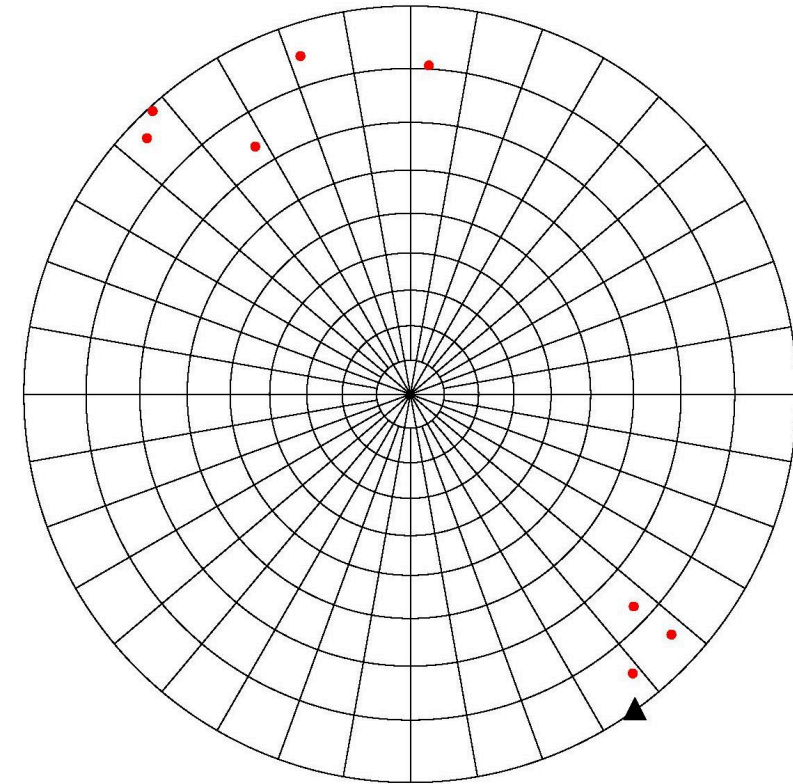
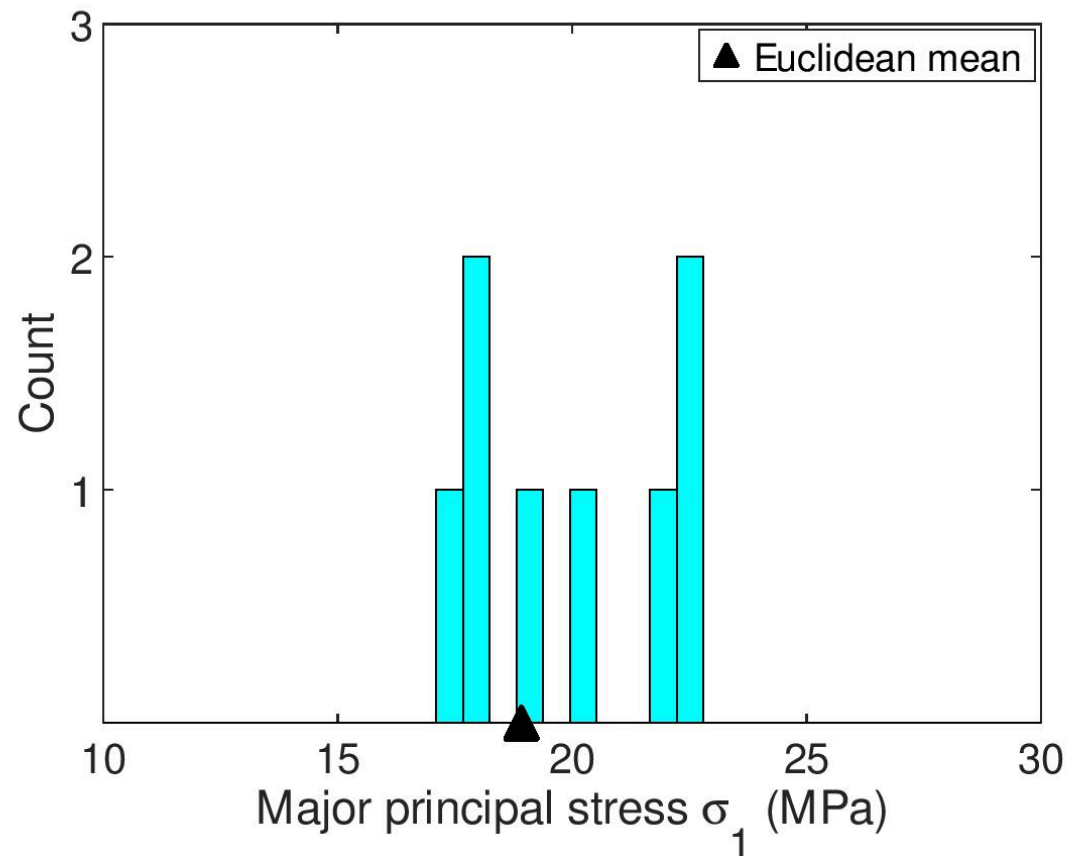
- Available data

| | Overcoring data | Hydraulic data |
|------------------------------|-----------------|----------------|
| Number of boreholes | 6 | 10 |
| Number of measurement points | 90 | 60 |
| Depth range [m] | 14-502 | 29-960 |



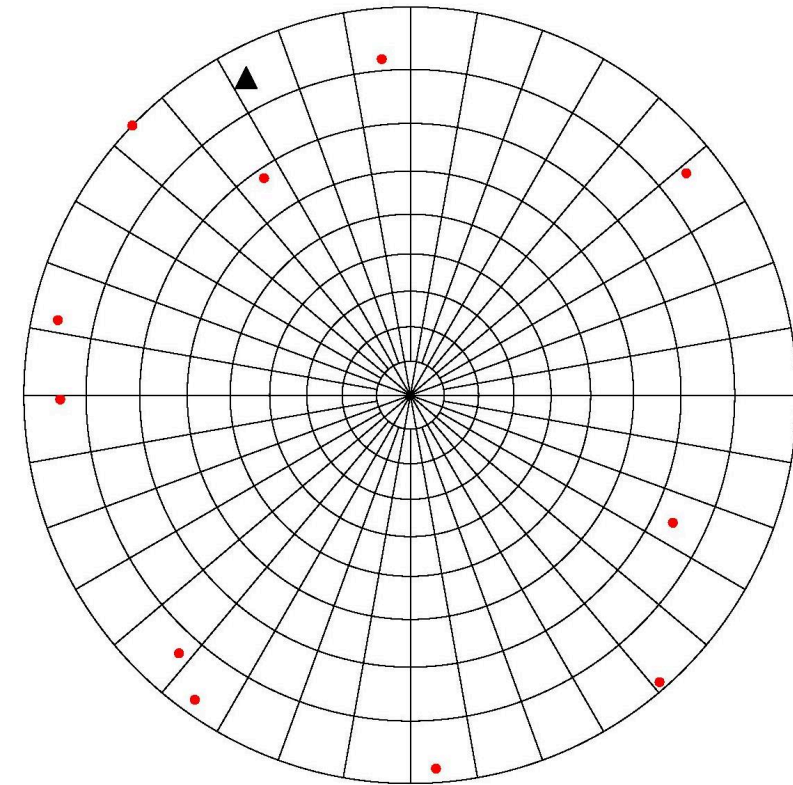
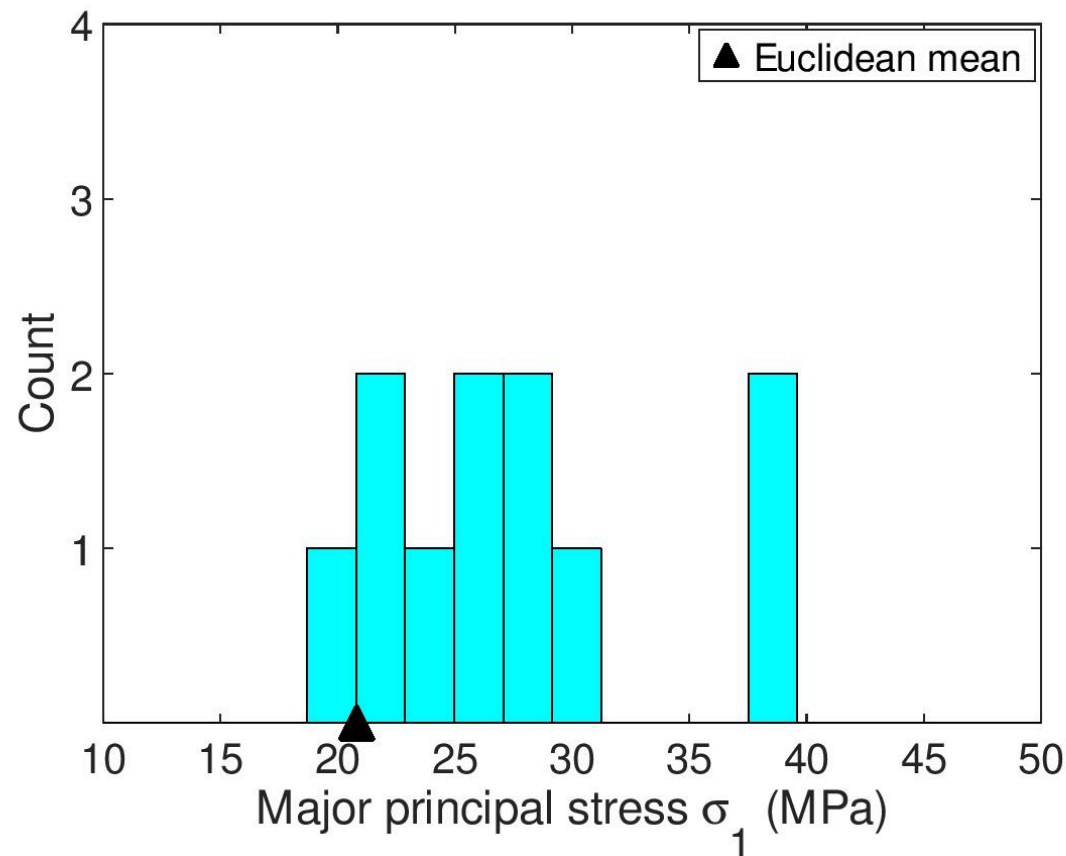
Results from stress measurement data (1/3)

- Selected data from borehole DBT3 (Depth range: 104-155 m, number = 8)
 - ❖ Magnitude and orientation of the major principal stress



Results from stress measurement data (2/3)

- Selected data from borehole KFM07C (Depth range: 158-197 m, number = 11)
 - ❖ Magnitude and orientation of the major principal stress



Results from stress measurement data (3/3)

- Correlation coefficients (Borehole DBT3)

| | σ_{xx} | σ_{xy} | σ_{xz} | σ_{yy} | σ_{yz} | σ_{zz} |
|---------------|---------------|---------------|---------------|---------------|---------------|---------------|
| σ_{xx} | 1.00 | -0.62 | 0.22 | -0.17 | 0.61 | 0.12 |
| σ_{xy} | -0.62 | 1.00 | -0.04 | 0.56 | -0.56 | 0.52 |
| σ_{xz} | 0.22 | -0.04 | 1.00 | 0.20 | -0.17 | 0.30 |
| σ_{yy} | -0.17 | 0.56 | 0.20 | 1.00 | -0.40 | 0.13 |
| σ_{yz} | 0.61 | -0.56 | -0.17 | -0.40 | 1.00 | 0.16 |
| σ_{zz} | 0.12 | 0.52 | 0.30 | 0.13 | 0.16 | 1.00 |

Borehole DBT3

| | σ_{xx} | σ_{xy} | σ_{xz} | σ_{yy} | σ_{yz} | σ_{zz} |
|---------------|---------------|---------------|---------------|---------------|---------------|---------------|
| σ_{xx} | 1.00 | 0.47 | 0.05 | 0.10 | 0.12 | 0.24 |
| σ_{xy} | 0.47 | 1.00 | 0.36 | 0.45 | 0.29 | 0.31 |
| σ_{xz} | 0.05 | 0.36 | 1.00 | 0.31 | -0.37 | -0.02 |
| σ_{yy} | 0.10 | 0.45 | 0.31 | 1.00 | 0.15 | 0.42 |
| σ_{yz} | 0.12 | 0.29 | -0.37 | 0.15 | 1.00 | 0.59 |
| σ_{zz} | 0.24 | 0.31 | -0.02 | 0.42 | 0.59 | 1.00 |

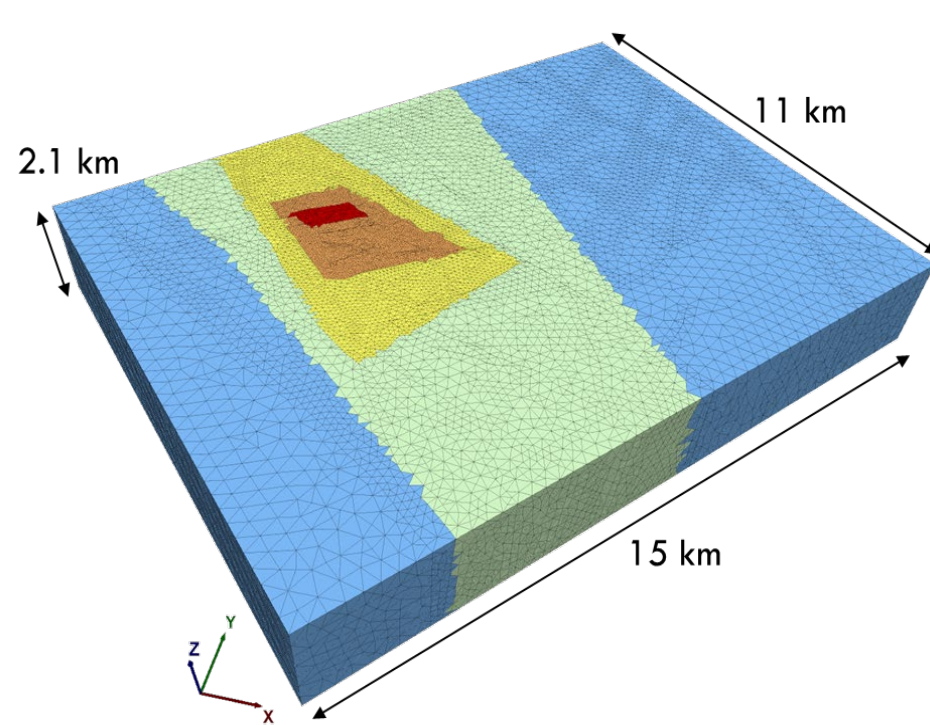
Borehole KFM07C

- Effective variance V_{eff} [MPa²]

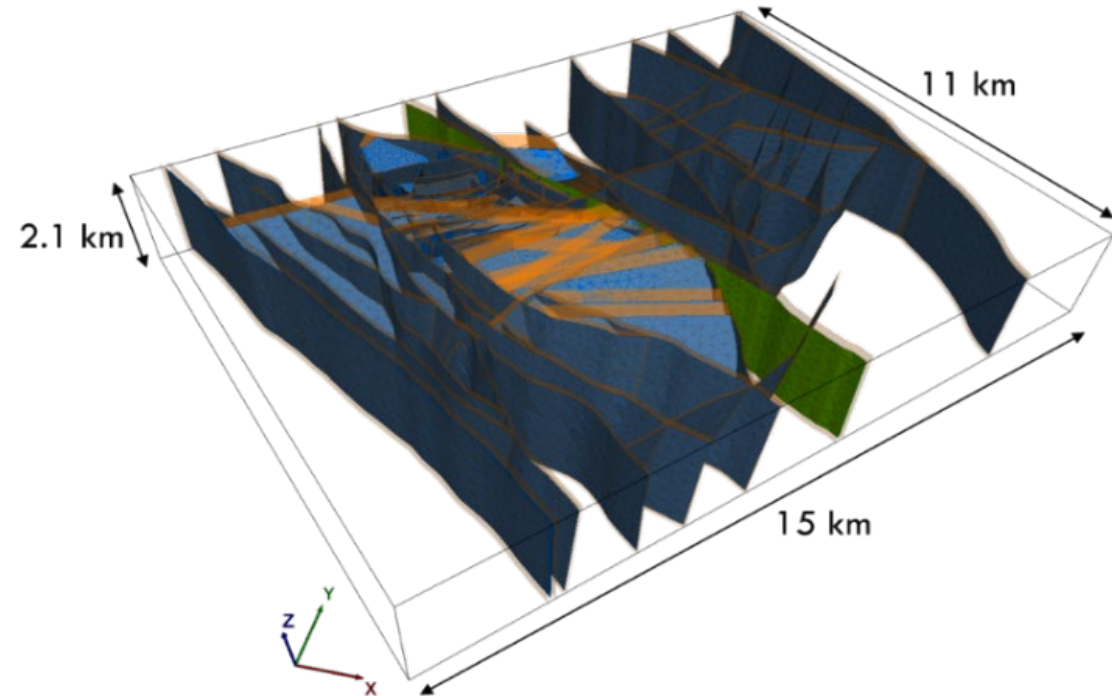
| Borehole | Fully tensorial | Quasi-tensorial |
|----------|-----------------|-----------------|
| DBT3 | 2.68 | 5.77 |
| KFM07C | 14.60 | 19.79 |

Application to the existing regional stress model (1/2)

- 3D regional stress model for Forsmark site



3DEC model

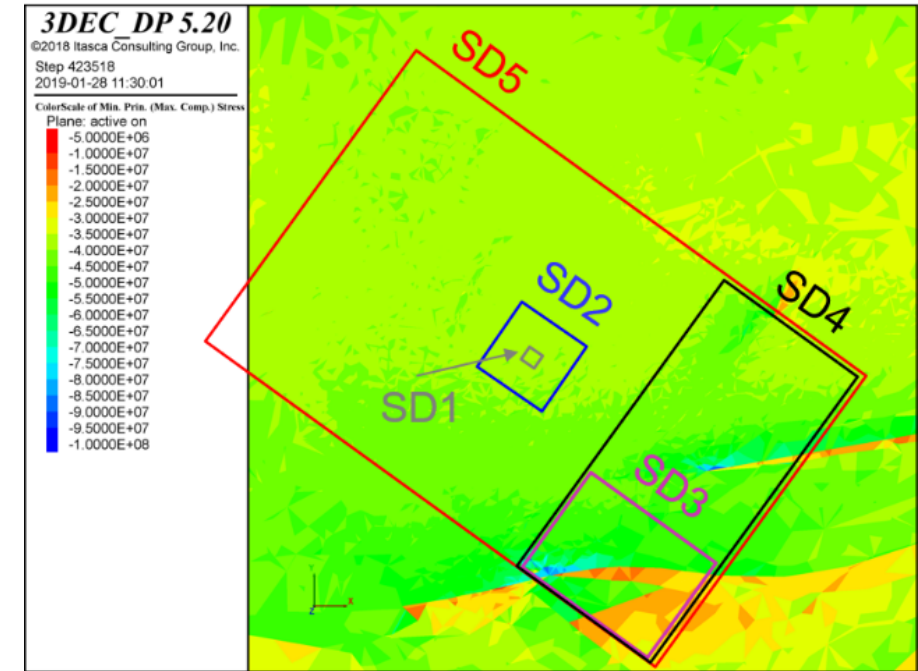


Undulating deformation zones represented by the blue, orange and green colors

Hakala, M., Ström, J., Valli, J., Juvani J. 2019. Stress-geology interaction modelling of the Forsmark site. Rock Mechanics Consulting Finland Oy.

Application to the existing regional stress model (2/2)

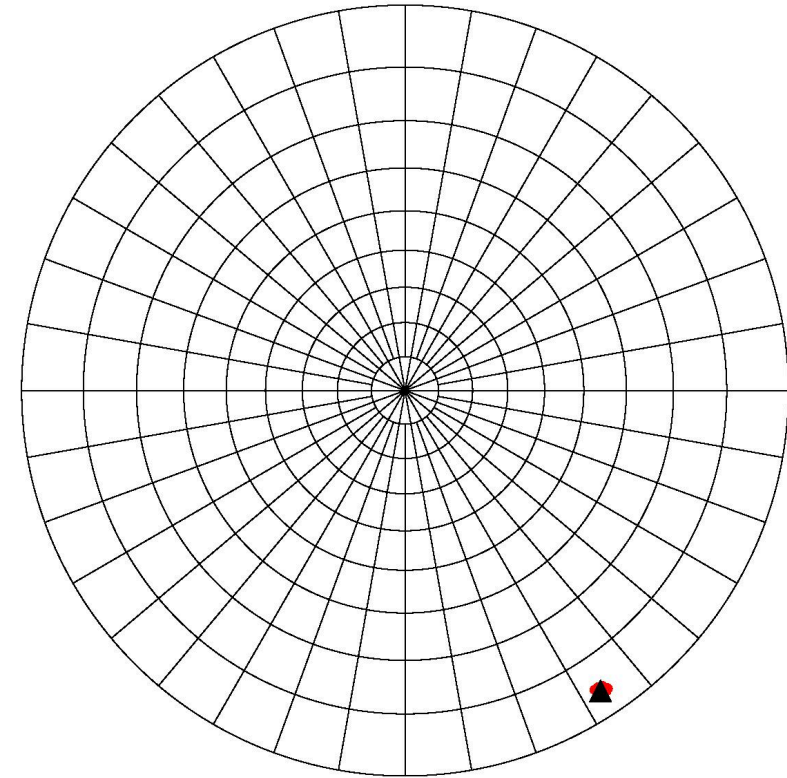
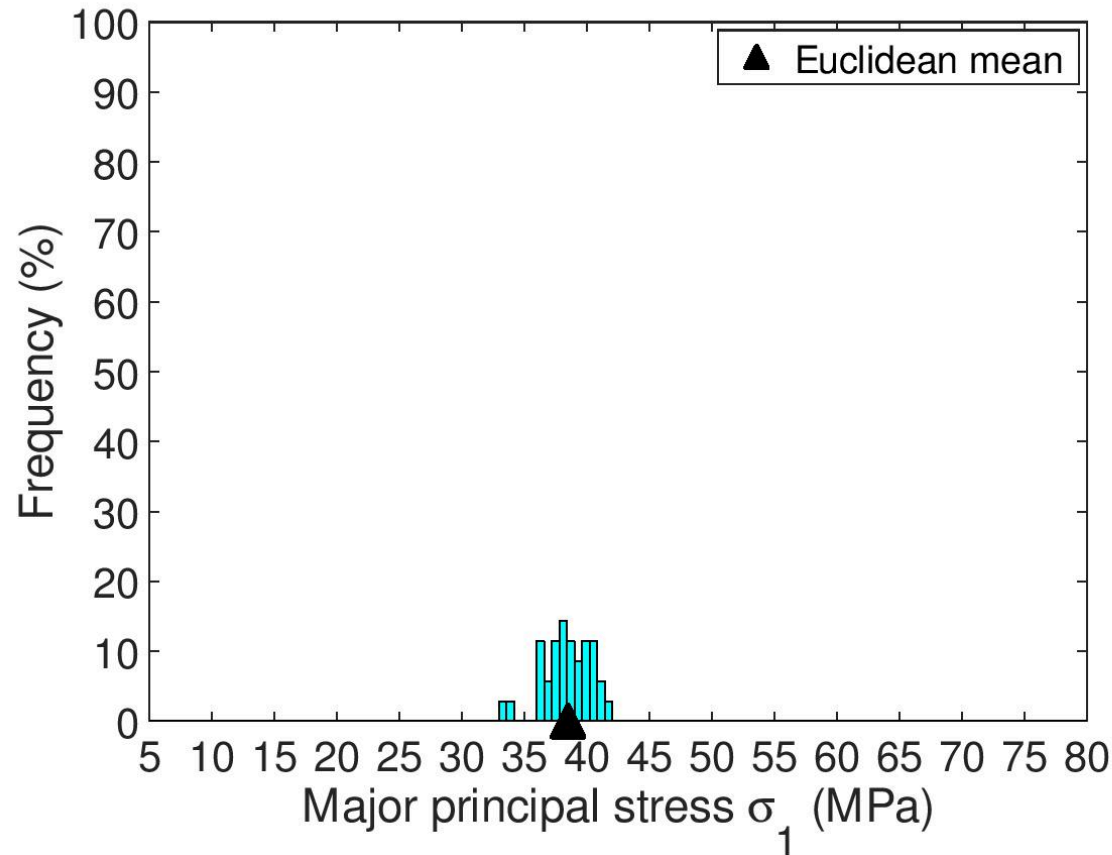
- Consideration of different sampling domains (SD) to evaluate the effects of the physical scale and number of data on the stress variability (slice with a thickness of 15 m)
 - ❖ SD1: drift scale (assumed stress homogeneity)
 - ❖ SD2: scale of hundreds of meters (assumed stress homogeneity)
 - ❖ SD3: scale of hundreds of meters (one region with stress heterogeneity identified in the contours of the principal stresses)
 - ❖ SD4: scale of hundreds of meters (two regions with stress heterogeneity identified in the contours of the principal stresses)
 - ❖ SD5: scale of the repository



Major principal stress

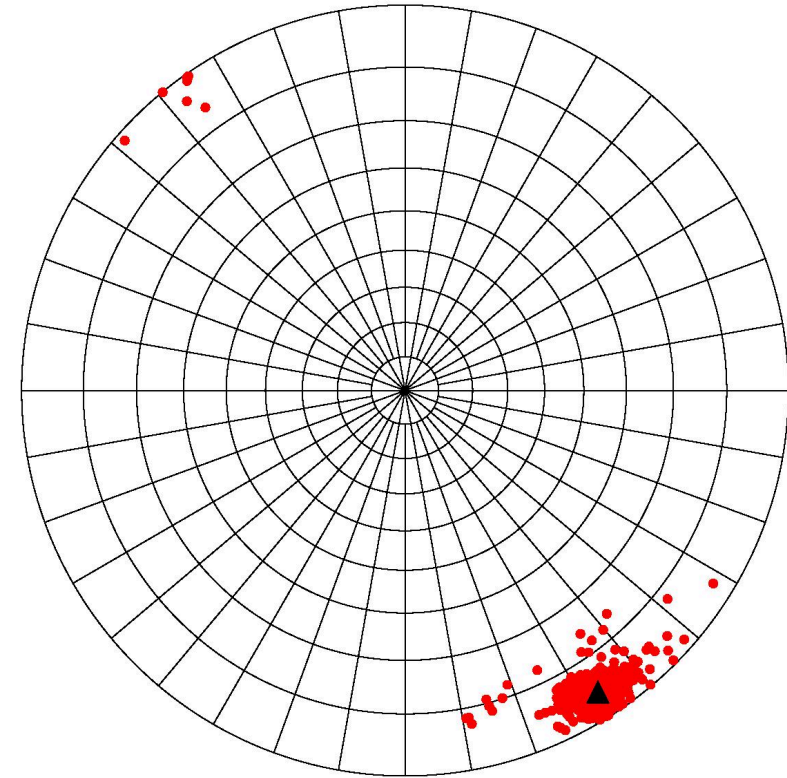
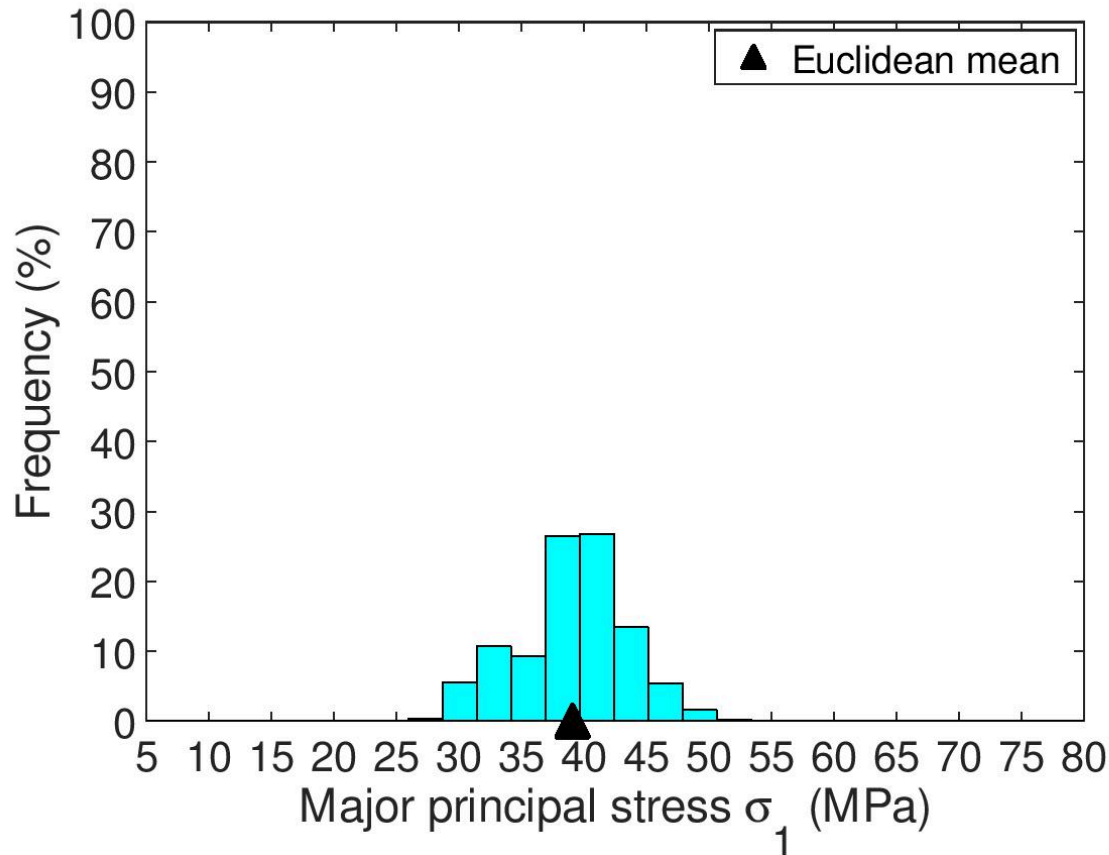
Results from the existing stress model (1/7)

- Magnitude and orientation of the major principal stress –SD1



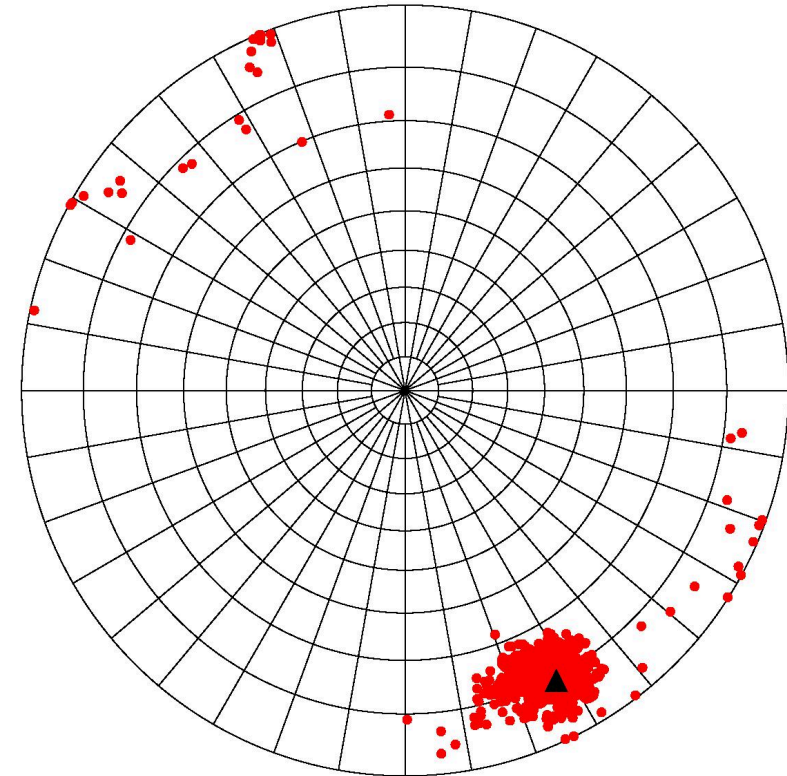
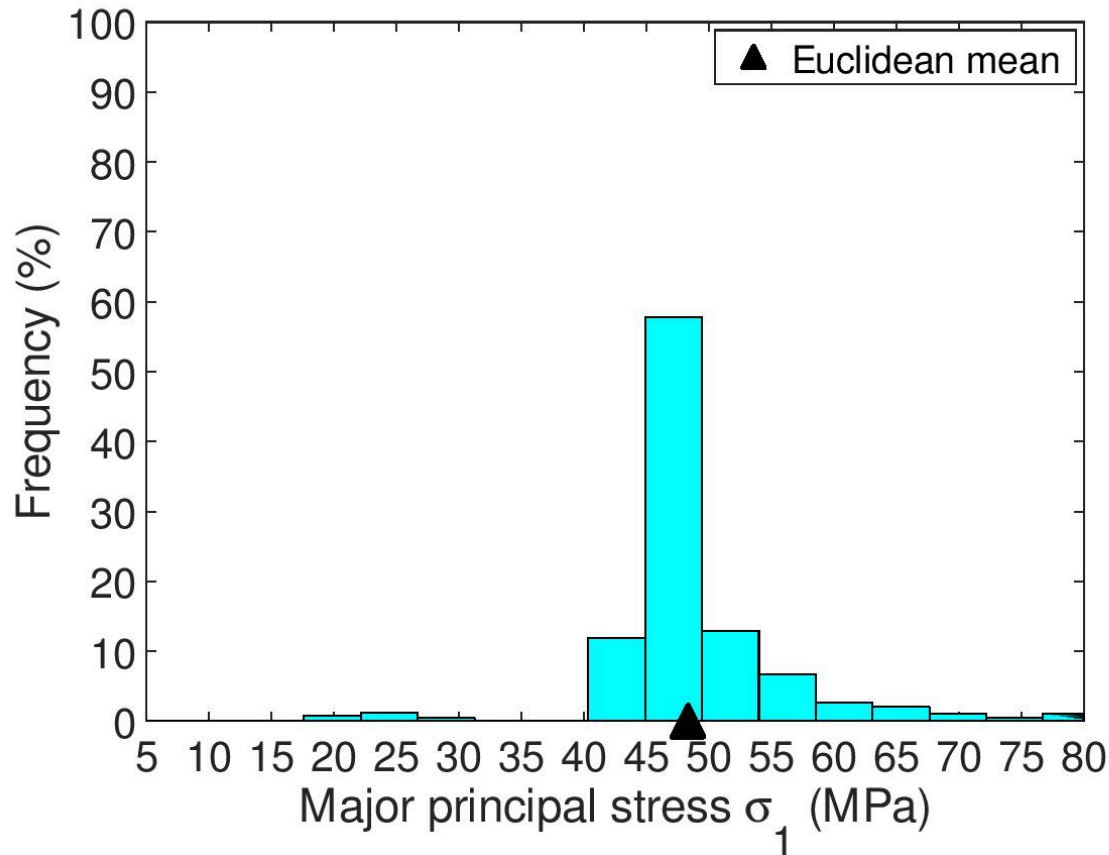
Results from the existing stress model (2/7)

- Magnitude and orientation of the major principal stress – SD2



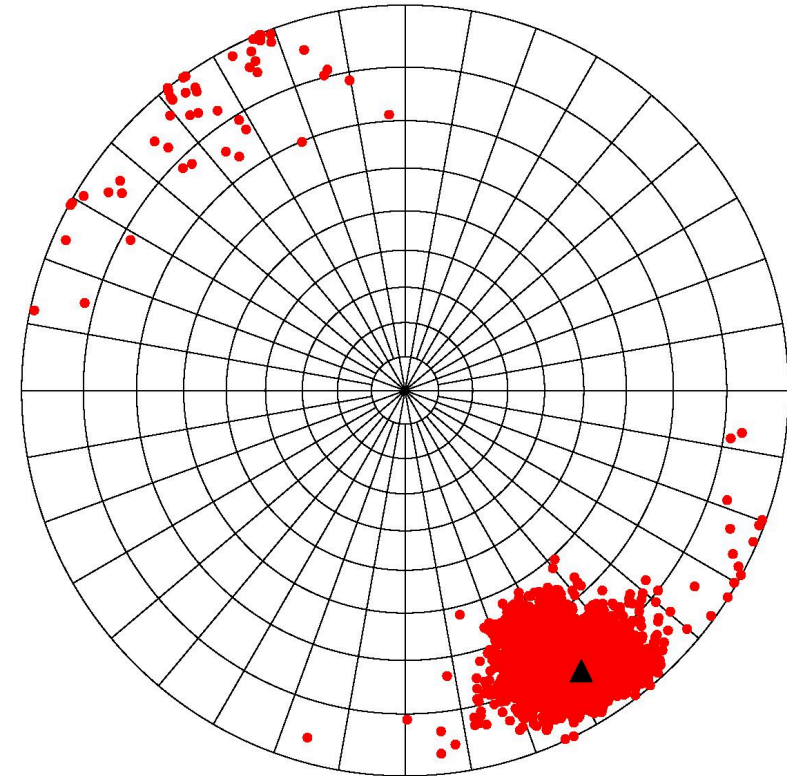
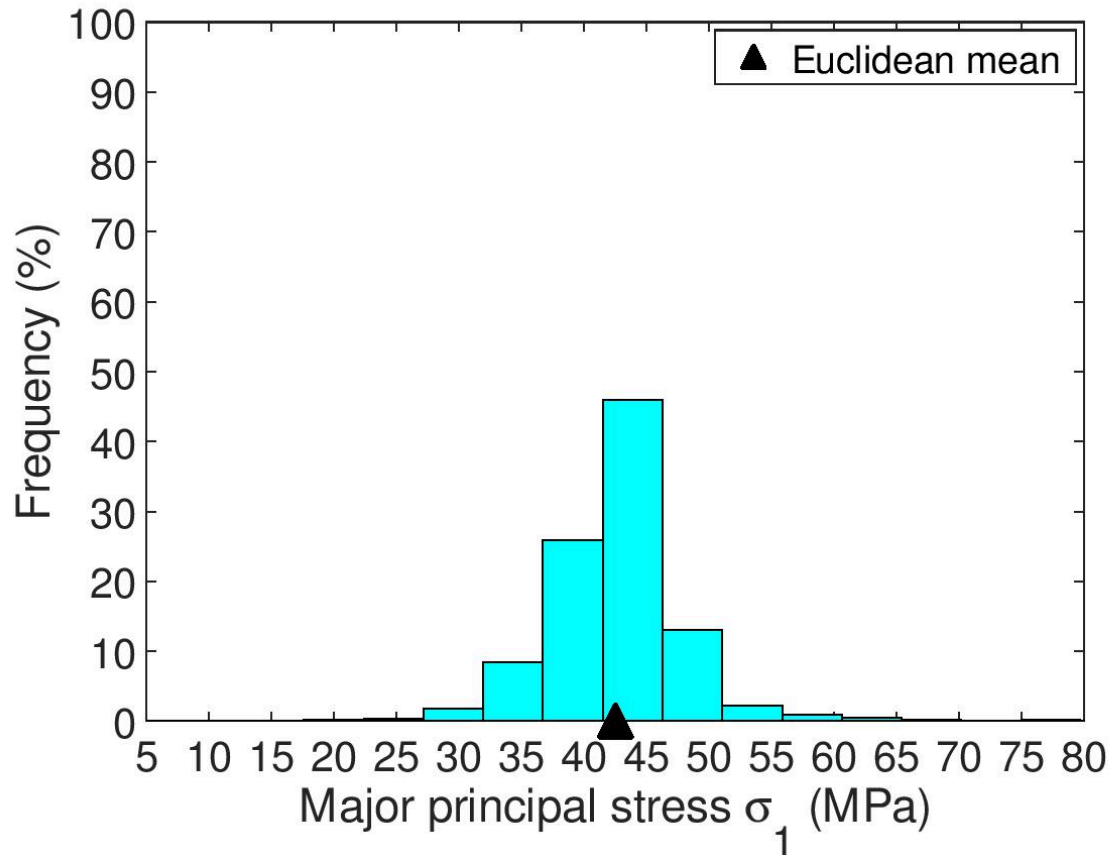
Results from the existing stress model (3/7)

- Magnitude and orientation of the major principal stress – SD3



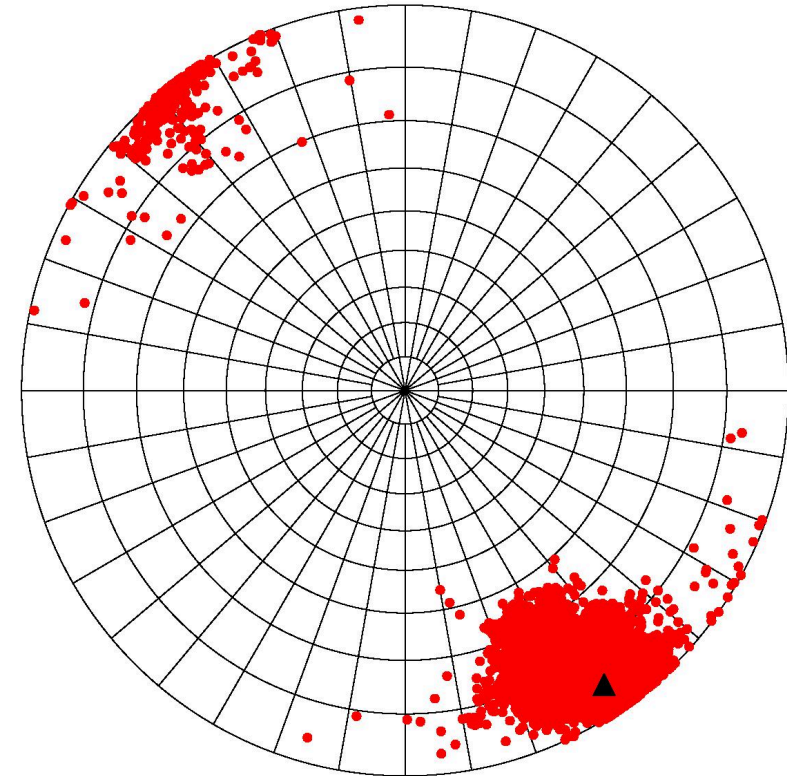
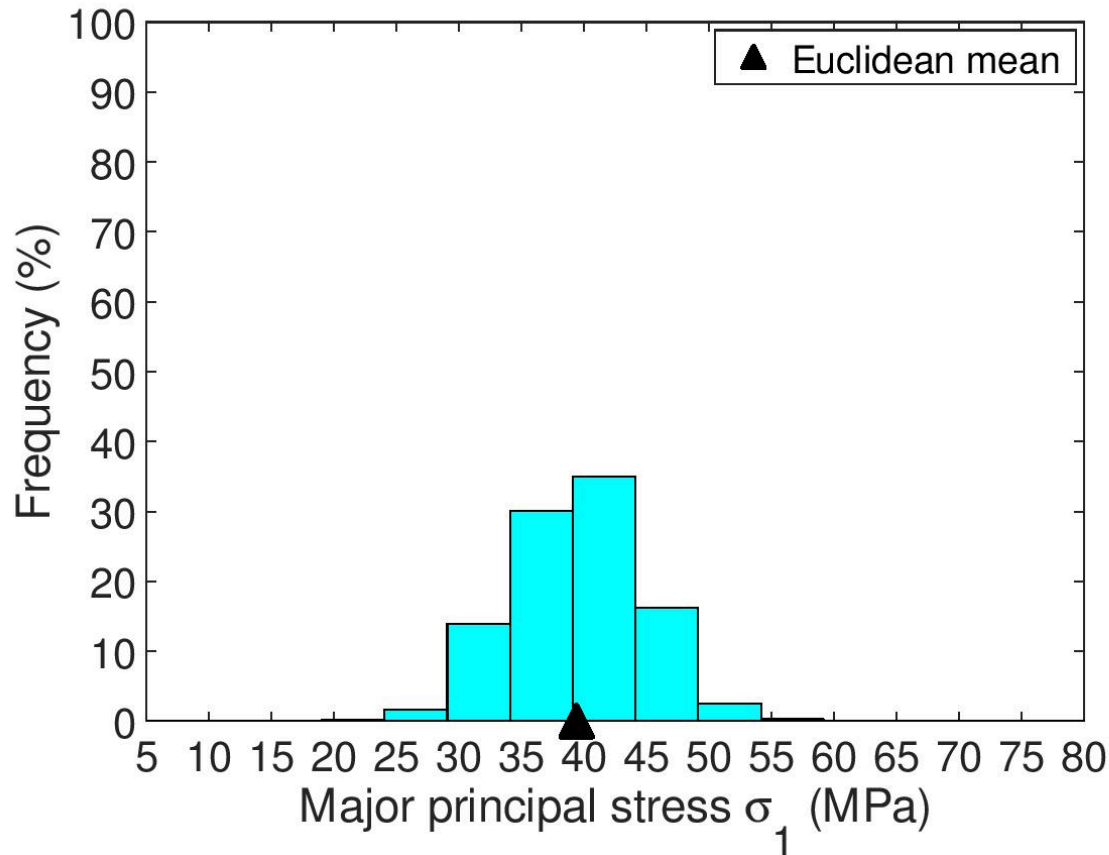
Results from the existing stress model (4/7)

- Magnitude and orientation of the major principal stress – SD4



Results from the existing stress model (5/7)

- Magnitude and orientation of the major principal stress – SD5



Results from the existing stress model (6/7)

- Matrix of the correlation coefficients

| | σ_{xx} | σ_{xy} | σ_{xz} | σ_{yy} | σ_{yz} | σ_{zz} |
|---------------|---------------|---------------|---------------|---------------|---------------|---------------|
| σ_{xx} | 1.00 | -0.80 | -0.29 | 0.96 | -0.62 | 0.97 |
| σ_{xy} | -0.80 | 1.00 | 0.23 | -0.79 | 0.43 | -0.71 |
| σ_{xz} | -0.29 | 0.23 | 1.00 | -0.37 | -0.36 | -0.27 |
| σ_{yy} | 0.96 | -0.79 | -0.37 | 1.00 | -0.54 | 0.95 |
| σ_{yz} | -0.62 | 0.43 | -0.36 | -0.54 | 1.00 | -0.61 |
| σ_{zz} | 0.97 | -0.71 | -0.27 | 0.95 | -0.61 | 1.00 |

Sampling domain SD2
(stress homogeneity)

| | σ_{xx} | σ_{xy} | σ_{xz} | σ_{yy} | σ_{yz} | σ_{zz} |
|---------------|---------------|---------------|---------------|---------------|---------------|---------------|
| σ_{xx} | 1.00 | -0.63 | -0.21 | 0.70 | 0.22 | 0.45 |
| σ_{xy} | -0.63 | 1.00 | 0.51 | -0.62 | -0.33 | 0.05 |
| σ_{xz} | -0.21 | 0.51 | 1.00 | -0.44 | -0.52 | 0.34 |
| σ_{yy} | 0.70 | -0.62 | -0.44 | 1.00 | 0.54 | 0.00 |
| σ_{yz} | 0.22 | -0.33 | -0.52 | 0.54 | 1.00 | -0.22 |
| σ_{zz} | 0.45 | 0.05 | 0.34 | 0.00 | -0.22 | 1.00 |

Sampling domain SD3
(stress heterogeneity)

Results from the existing stress model (7/7)

- Overall stress field dispersion

| SD | Effective variance V_{eff} [MPa ²] | | | |
|-----|---|------|------|------|
| | Depth (m) | | | |
| | 300 | 450 | 470 | 500 |
| SD1 | 0.02 | 0.04 | 0.04 | 0.01 |
| SD2 | 0.48 | 0.44 | 0.45 | 0.49 |
| SD3 | 5.30 | 6.60 | 4.43 | 4.31 |
| SD4 | 7.46 | 3.88 | 2.82 | 2.56 |
| SD5 | 3.53 | 1.82 | 1.72 | 1.65 |

Fully tensorial approach

| SD | Effective variance V_{eff} [MPa ²] | | | |
|-----|---|-------|------|------|
| | Depth (m) | | | |
| | 300 | 450 | 470 | 500 |
| SD1 | 0.10 | 0.26 | 0.27 | 0.08 |
| SD2 | 2.74 | 1.91 | 1.84 | 2.01 |
| SD3 | 16.68 | 14.51 | 7.30 | 6.76 |
| SD4 | 13.58 | 7.58 | 5.10 | 4.76 |
| SD5 | 6.63 | 4.63 | 4.32 | 4.12 |

Quasi-tensorial approach

Conclusions

- The various stress tensor components are significantly correlated.
- The stress dispersion obtained with a quasi-tensorial approach is overestimated and hence, not exclusively related with the stress heterogeneity.
- When the fully tensorial approach is applied to stress measurement data, the division in several data sets or a large number of data may be needed.
- When the fully tensorial approach is applied to numerical modelling results:
 - ❖ A large number of stress data at any depth can be considered;
 - ❖ The stress dispersion of several sampling domains and depth intervals can be quantified;
 - ❖ It can assist in the design of future stress measurement campaigns; and
 - ❖ The overall stress dispersion is smaller than that obtained from data analysis.

Acknowledgement

- The authors gratefully acknowledge the Swedish Nuclear Fuel and Waste Management Company for providing financial support to research presented and Diego Mas Ivars (co-author), for many helpful discussions.