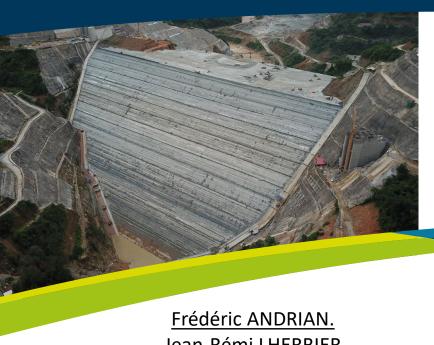
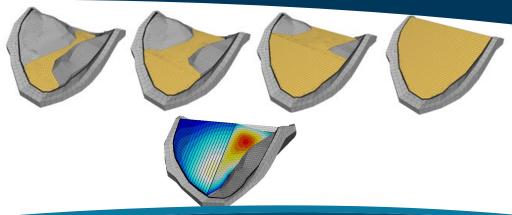
# Verification of the mitigation measures for preventing the concrete face failure of a 210m CFRD





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#### DAM DESCRIPTION

💶 480 MW HPP Scheme in Laos – Nam Ngum river 🤇

ARTELIA Owner's Engineer for EDL

210 m high, 520 m crest length

Upstream slope 1.4 H / 1 V

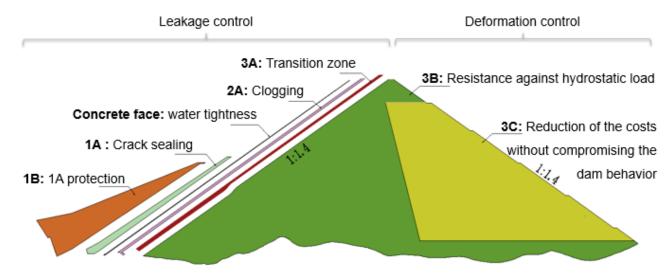
Downstream slope 1.5 H / 1V (including berms)

Foundation: sandstones and conglomerates





#### **DAM ZONING**

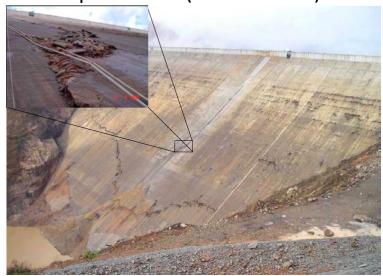


- 3B fresh gneiss (70%), 3C moderately weathered gneiss (90%)
- Maximum particle size: 800mm (~lift thickness)

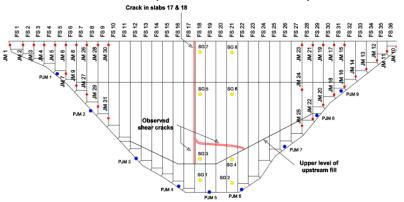


#### FAILURE FEEDBACK ON HIGH CFRDs

Campos Novos (202m -Brazil)



### Mohale (145m -Lesotho)



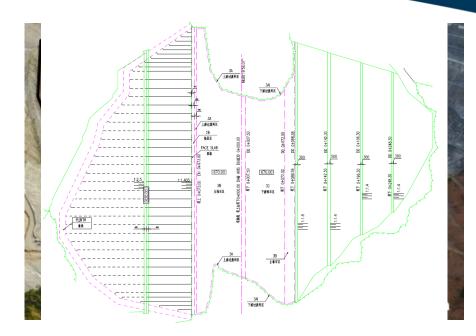


Concrete face under prescribed displacement



#### A VERY PECULIAR VALLEY SHAPE

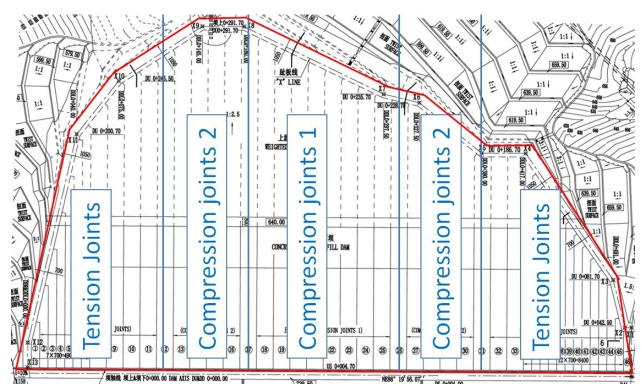
- Concrete face constructed slightly upstream the narrowest part of the valley
  - Probably for rockfill volume saving
- High stiffness contrast between the side and the central part of rockfill
  - Behavior at the impounding?



Cross spections at view20



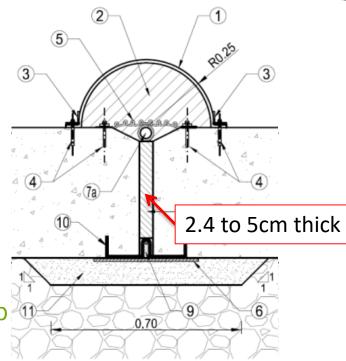
#### **CONCRETE FACE LAYOUT**





#### **CONCRETE FACE LAYOUT**

- 46 panels
  - From ~ 30 to 100 cm at the dam toe
- Joints
  - Tension joints
  - Compression joints 1: 5cm initial gap
  - Compression joints 2: 2.4cm initial gap



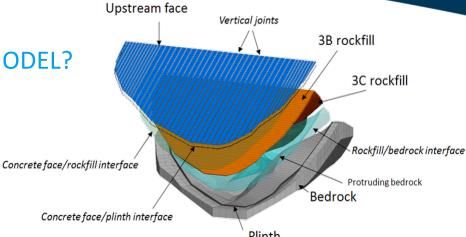
Confrenceisosniojo ijrotint



### **Numerical model**

**OWNER'S ENGINEER NUMERICAL MODEL?** 

Existing Contractor's numerical model



FLAC 3D numerical model

- ARTELIA's verification model with major improvements
  - A more rational assessment of scale effect
  - A better simulation of rockfill / bedrock interface
  - Initial gap of compression joints taken into account
  - Delayed deformation based on international feedback and laboratory tests

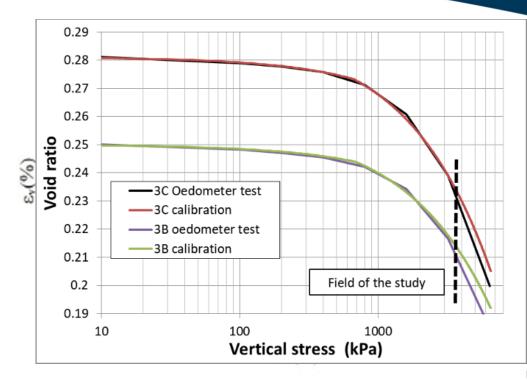
### **Constitutive laws**

#### **ROCKFILL**

- 3B and 3C zones modeled (PHM)
- Shear + Volumetric hardening
- Consideration of a stressdependent friction angle

$$\Phi = \Phi_0 - \Delta\phi \log \left(\frac{-\sigma_3}{p_{ref}}\right)$$

Good calibration with laboratory tests



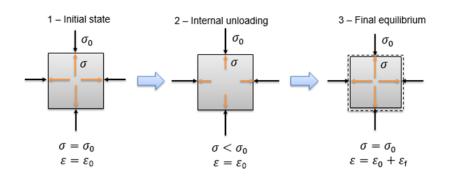
Triaxial - Diletancy
OEdometer

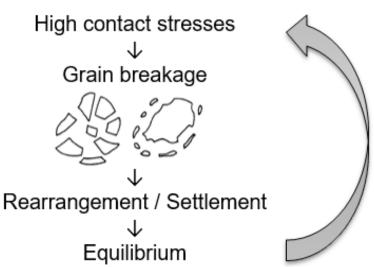


# **Delayed deformation**

#### MAIN PRINCIPLES

- Viscosity brought by
  - Saturation
  - Fine materials
- Delayed deformation
  - → stress relaxation in the model







### **Delayed deformation**

### **ANALYTICAL FORMULATION (SHEN 1991)**

Long-term volumetric strain

$$\varepsilon_{vf} = b \left( \frac{\sigma_3}{p_a} \right)^{m_1} + c \left( \frac{q}{p_a} \right)^{m_2}$$

Long-term deviatoric strain

$$\{\epsilon f\} = \epsilon_{V,f} * \frac{\{I\}}{3} + \gamma_f * \frac{\{S\}}{q}$$

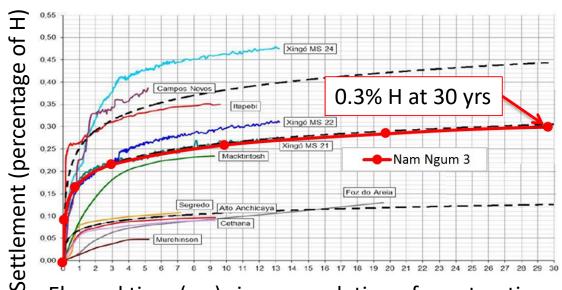
$$\gamma_f = d \left( \frac{S_l}{1 - S_l} \right)^{m_3}$$

 b, c, d, m1, m2 and m3 material parameters calibrated by means of laboratory tests

### **Delayed deformation**

#### **CHOICE FOR NAM NGUM 3**

- Average delayed settlement chosen for Nam Ngum 3 dam
  - Based on international feedback (CBDB)
  - Calibrated from laboratory test (stress dependency)



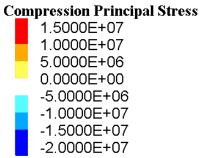
Elapsed time (yrs) since completion of construction

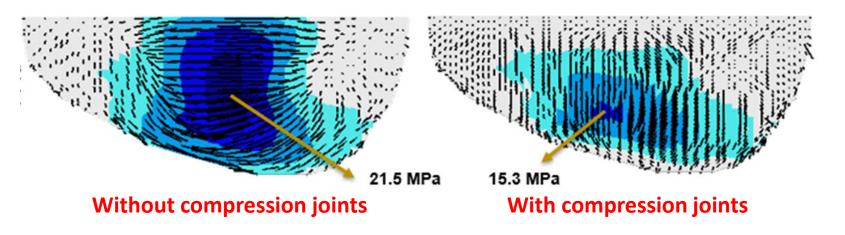


### Results

#### STRESSES IN CONCRETE FACE

- Clear beneficial effects of the compression joints
  - After 30 years of operation



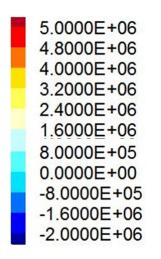


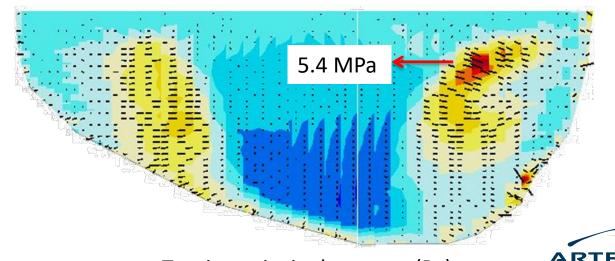


### Results

#### STRESSES IN CONCRETE FACE

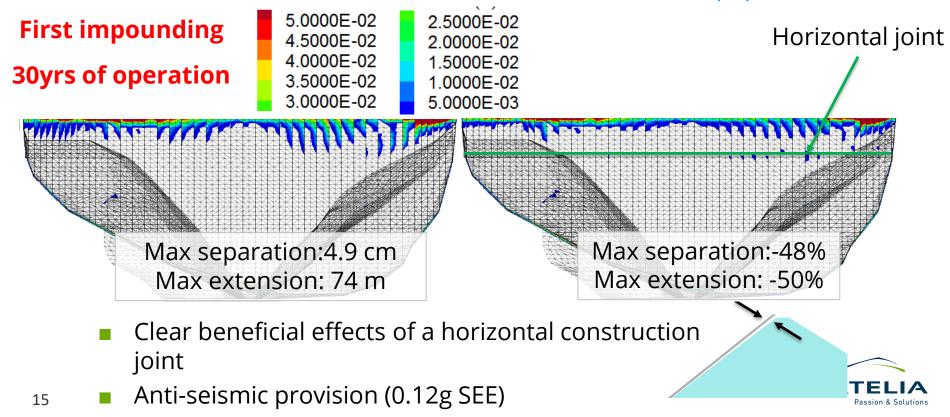
- Diagonal tensile stresses due to the valley shape after 30 years of operation
  - → Structural rebar reinforcement to be provided





### Results

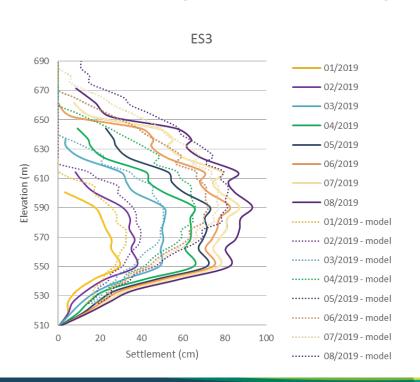
### DETACHMENT BETWEEN CONCRETE FACE AND ROCKFILL (M)



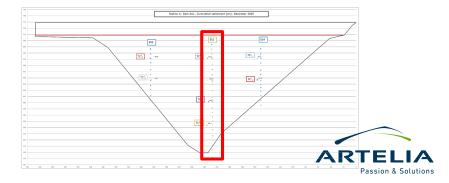
# Calibration on the monitoring data

### **REASSURING BEHAVIOR**

Electromagnetic settlement gauges



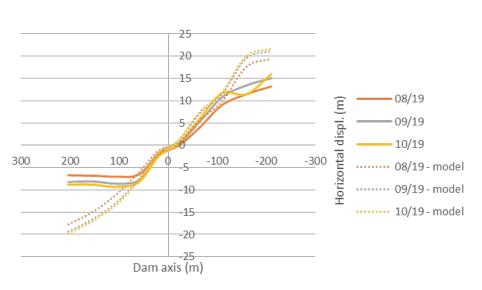


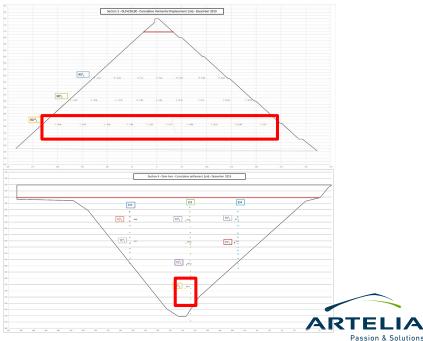


# Calibration on the monitoring data

#### **REASSURING BEHAVIOR**

Horizontal displacement gauges





# Calibration on the monitoring data

### Reassuring behavior

- Compaction: 10 passes of 26t vibrating roller (almost twice as usual)
- 3C zone replaced by 3B very early in the construction
- Apparent Young's modulus: 80 MPa expected, 150-180 MPa measured
  - Decreased risk of cracking

